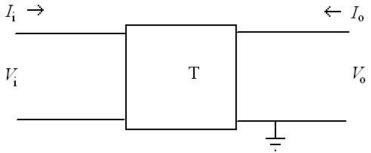
Lecture 7: Transistors and Amplifiers

Hybrid Transistor Model for small AC :

- The previous model for a transistor used one parameter (β , the current gain) to describe the transistor.
 - doesn't explain many features of three common forms of transistor amplifiers (common emitter etc.)
 - e.g. could not calculate the output impedance of the common emitter amp.
- Very often in electronics we describe complex circuits in terms of an equivalent circuit or model.
 - need a model that relates the input currents and voltages to the output currents and voltages.
 - the model needs to be linear in the currents and voltages.
 - For a transistor this condition of linearity is true for *small* signals.
- The most general linear model of the transistor is a 4-terminal "black box".



- In this model we assume the transistor is biased on properly and do not show the biasing circuit.
- Since a transistor has only 3 legs, one of the terminals is common between the input and output.
- There are 4 variables in the problem, I_i , V_i , I_o , and V_o .
 - The subscript i refer to the input side while the subscript o refers to the output side.
 - We assume that we know I_i and V_o .

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• Kirchhoff's laws relate all the currents and voltages:

$$V_{i} = V_{i}(I_{i}, V_{o})$$
$$I_{o} = I_{o}(I_{i}, V_{o})$$

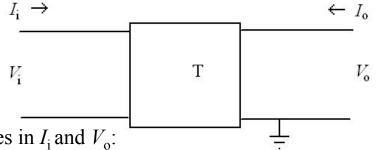
• For a linear model of the transistor with a small changes in I_i and V_o :

$$dV_{i} = \left(\frac{\partial V_{i}}{\partial I_{i}}\right)_{V_{o}} dI_{i} + \left(\frac{\partial V_{i}}{\partial V_{o}}\right)_{I_{i}} dV_{o}$$
$$dI_{o} = \left(\frac{\partial I_{o}}{\partial I_{i}}\right)_{V_{o}} dI_{i} + \left(\frac{\partial I_{o}}{\partial V_{o}}\right)_{I_{i}} dV_{o}$$

• The partial derivatives are called the hybrid (or *h*) parameters:

$$dV_{i} = h_{ii}dI_{i} + h_{io}dV_{o}$$
$$dI_{o} = h_{oi}dI_{i} + h_{oo}dV_{o}$$

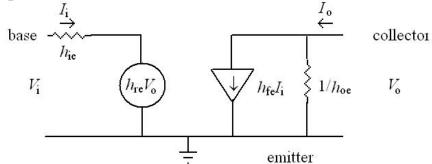
- h_{oi} and h_{io} are unitless
- h_{oo} has units $1/\Omega$ (mhos)
- h_{ii} has units Ω
- The four *h* parameters are easily measured.
 - e.g. to measure h_{ii} hold V_o (the output voltage) constant and measure V_{in}/I_{in} .
- Unfortunately the *h* parameters are not constant.
 - e.g. Figs. 11-14 of the 2N3904 spec sheet show the variation of the parameters with $I_{\rm C}$.



- There are 3 sets of the 4 hybrid parameters.
 - One for each type of amp: common emitter, common base, common collector ٠
 - In order to differentiate one set of parameters from another the following notation is used: ٠
 - **First subscript** Second subscript
 - i = input impedance e = common emitter
 - o = output admittance b = common base
 - r = reverse voltage ratio c = common collector
 - f = forward current ratio
 - For a common emitter amplifier we would write: B

$$dV_{i} = h_{ie} dI_{i} + h_{re} dV_{o}$$
$$dI_{o} = h_{fe} dI_{i} + h_{oe} dV_{o}$$

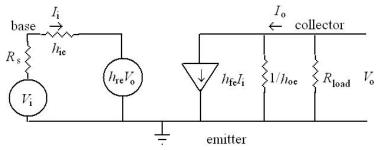
- Typical values for the *h* parameters for a 2N3904 transistor in the common emitter configuration:
 - $h_{\rm fe} = 120, h_{\rm oe} = 8.7 \times 10^{-6} \,\Omega^{-1}, h_{\rm ie} = 3700 \,\Omega, h_{\rm re} = 1.3 \times 10^{-4} \,\text{for} \,I_{\rm C} = 1 \,\text{mA}$
- The equivalent circuit for a transistor in the common emitter configuration looks like:



- Circle: voltage source
 - the voltage across this element is always equal to $h_{\rm re}V_0$ independent of the current through it.
- Triangle: current source ٠
 - the current through this element is always $h_{fe}I_{in}$ independent of the voltage across the device. L7: Transistors and Amplifiers

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- We can use the model to calculate voltage/current gain and the input/output impedance of a CE amp.
- Equivalent circuit for a CE amp with a voltage source (with resistance R_s) and load resistor (R_{load}):



biasing network not shown

- **Current gain**: $G_{\rm I} = I_{\rm o}/I_{\rm in}$
 - Using Kirchhoff's current law at the output side we have:

$$h_{\rm fe}I_{\rm in} + V_{\rm o}h_{\rm oe} = I_{\rm o}$$

• Using Kirchhoff's voltage rule at the output we have:

$$V_{o} = -I_{o}R_{load}$$

$$h_{fe}I_{in} = h_{oe}I_{o}R_{load} + I_{o}$$

$$G_{I} = I_{o} / I_{in} = h_{fe} / (1 + h_{oe}R_{load})$$

- For typical CE amps, $h_{oe}R_{load} \ll 1$ and the gain reduces to familiar form: $G_{I} \approx h_{fe} = \beta$
- Voltage gain: $G_v = V_o/V_{in}$
 - This gain can be derived in a similar fashion as the current gain:

$$G_{\rm V} = V_{\rm o} / V_{\rm in} = -h_{\rm fe} R_{\rm load} / (\Delta R_{\rm load} + h_{\rm ie})$$

h \Lambda = h \cdot h \cdot - h_{\rm c} h \cdot \vee 10^{-2}

with $\Delta = h_{ie}h_{oe} - h_{fe}h_{re} \approx 10^{-2}$ This reduces to a familiar form f

This reduces to a familiar form for most cases where $\Delta R_{\text{load}} \ll h_{\text{ie}}$ $G_{\text{V}} = -h_{\text{fe}}R_{\text{load}} / h_{\text{ie}} = -R_{\text{load}} / r_{\text{BE}}$ L7: Transistors and Amplifiers

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• **Input Impedance**: $Z_i = V_{in}/I_{in}$

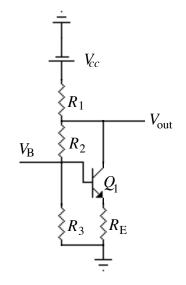
 $Z_{\rm i} = (\Delta R_{\rm load} + h_{\rm ie})/(1 + h_{\rm oe}R_{\rm load})$

- This reduces to a familiar form for most cases where $\Delta R_{\text{load}} \ll h_{\text{ie}}$ and $h_{\text{oe}} R_{\text{load}} \ll 1$ $Z_{\text{i}} = h_{\text{ie}} = h_{\text{fe}} r_{\text{BE}}$
- $Z_{i} = h_{ie} = h_{fe} r_{BE}$ • Output Impedance: $Z_{o} = V_{o}/I_{o}$ $Z_{o} = (R_{s} + h_{ie})/(\Delta + h_{oe}R_{s})$
 - Z_{o} does not reduce to a simple expression.
 - As the denominator is small, Z_0 is as advertised large.

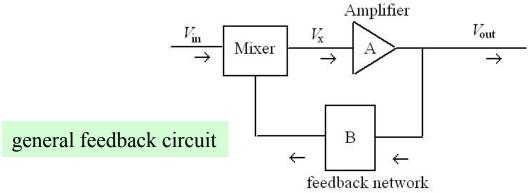
Feedback and Amplifiers

- Consider the common emitter amplifier shown.
 - This amp differs slightly from the CE amp we saw before:
 - bias resistor R_2 is connected to collector resistor R_1 instead of directly to V_{cc} .
 - How does this effect V_{out} ?
 - If V_{out} decreases (moves away from V_{cc})
 - \square I_2 increases
 - \sim V_B decreases (gets closer to ground)
 - $\sim V_{\text{out}}$ will increase since $\Delta V_{\text{out}} = -\Delta V_{\text{B}} R_1 / R_{\text{E}}$
 - If V_{out} increases (moves towards V_{cc})
 - \square I_2 decreases
 - \sim V_B increases (moves away from ground).
 - V_{out} will decrease since $\Delta V_{\text{out}} = -\Delta V_{\text{B}} R_{1}/R_{\text{E}}$

This is an example of NEGATIVE FEEDBACK



- Negative Feedback is good:
 - Stabilizes amplifier against oscillation
 - Increases the input impedance of the amplifier
 - Decreases the output impedance of the amplifier
- Positive Feedback is bad:
 - Causes amplifiers to oscillate
- Feedback Fundamentals:



• Without feedback the output and input are related by:

 $V_{\text{out}} = AV_{\text{in}}$

- The feedback (box B) returns a portion of the output voltage to the amplifier through the "mixer".
 - The feedback network on the AM radio is the collector to base resistors (R_3, R_5)
- The input to the amplifier is:

$$V_{\rm x} = V_{\rm in} + BV_{\rm out}$$

• The gain with feedback is:

$$V_{\text{out}} = AV_{\text{x}} = A(V_{in} + BV_{\text{out}})$$

$$G = V_{\text{out}} / V_{\text{in}} = A / (1 - AB)$$

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A: open loop gain*AB*: loop gain*G*: closed loop gain

Oscillation is a large fluctuation of output signal with no input

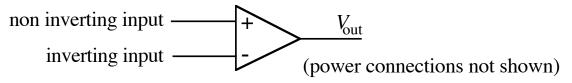
- Positive and negative feedback:
 - Lets define A > 0 (positive)
 - $G = V_{out} / V_{in} = A / (1 AB)$ Positive feedback, AB > 0:
 - - As $AB \rightarrow 1, G \rightarrow \infty$.
 - circuit is unstable
 - oscillates if AB = 1
 - Negative feedback, AB < 0:
 - As $A \rightarrow \infty$, an amazing thing happens: $|AB| \rightarrow \infty$
 - $|G| \rightarrow |1/B|$

For large amplifier gain (A) the circuit properties are determined by the feedback loop.

- Example: $A = 10^5$ and B = -0.01 then G = 100.
- The stability of the gain is determined by the feedback loop (B) and not the amplifier (A).
- Example: *B* is held fixed at 0.01 and *A* varies:
 - Gain A
 - $5x10^3$ 98.3
 - 1×10^4 99.0
 - $2x10^4$ 99.6
 - circuits can be made stable with respect to variations in the transistor characteristics B as long as *B* is stable.
 - *B* can be made from precision components such as resistors. \bigcirc

Operational Amplifiers (Op Amps)

- Op amps are very high gain ($A = 10^5$) differential amplifiers.
 - Differential amp has two inputs (V_1, V_2) and output $V_{out} = A (V_1 V_2)$ where A is the amplifier gain.



- If an op amp is used without feedback and $V_1 \neq V_2$
 - \sim $V_{\rm out}$ saturates at the power supply voltage (either positive or negative supply).
- Example: Assume the maximum output swing for an op amp is ± 15 V.
 - If there is no feedback in the circuit:

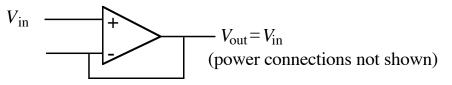
$$V_{out} = 15 \text{ V if } V_{non-invert} > V_{invert}$$

$$V_{out} = -15 \text{ V if } V_{non-invert} < V_{invert}$$

- Op amps are almost always used with negative feedback.
 - The output is connected to the (inverting) input.
- Op amps come in "chip" form. They are made up of complex circuits with 20-100 transistors.

Ideal Op Amp		Real Op Amp μA741	
Voltage gain (open loop)	∞	10 ⁵	
Input impedance	∞	2 MΩ	
Output impedance	0	$75 \ \Omega$	
Slew rate	∞	0.5 V/µsec	Slew rate is how fast output can change
Power consumption	0	50 mW	
V_{out} with $V_{in} = 0$	0	2 mV (unity gain)	
Price	0\$	\$0.25	
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- When working with op amps using negative feedback two simple rules (almost) always apply:
 - No current goes into the op amp.
 - This reflects the high input impedance of the op amp.
 - Both input terminals of the op amp have the same voltage.
 - This has to do with the actual circuitry making up the op amp.
- Some examples of op amp circuits with negative feedback:
 - Voltage Follower:

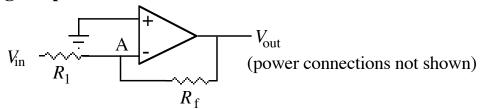


- The feedback network is just a wire connecting the output to the input.
- By rule #2, the inverting (-) input is also at V_{in} .

$$V_{\text{out}} = V_{\text{in}}.$$

- What good is this circuit?
 - Mainly as a buffer as it has high input impedance (M Ω) and low output impedance (100 Ω).

• Inverting Amplifier:



- By rule #2, point A is at ground.
- By Rule #1, no current is going into the op amp.
- We can redraw the circuit as:

$$V_{\rm m} \xrightarrow{I_{\rm in}} \xrightarrow{R_{\rm f}} V_{\rm out}$$

$$V_{\rm m} \xrightarrow{R_{\rm f}} V_{\rm out}$$

$$V_{\rm in} / R_{\rm 1} + V_{\rm out} / R_{\rm f} = 0$$

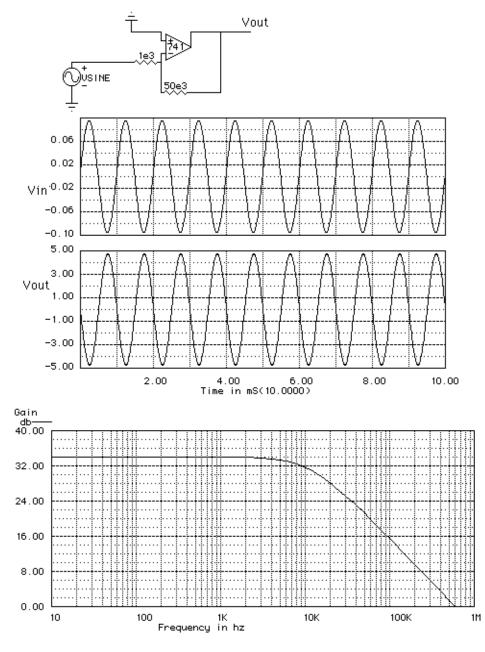
$$V_{\rm out} / V_{\rm in} = -R_{\rm f} / R_{\rm 1}$$

$$V_{\rm in} = R_{\rm f} / R_{\rm 1}$$

$$V_{\rm in} = R_{\rm f} / R_{\rm 1}$$

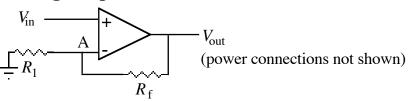
$$V_{\rm in} = R_{\rm f} / R_{\rm 1}$$

• The minus sign in the gain means that the output has the opposite polarity as the input.



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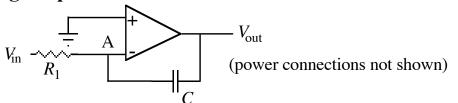
• Non-Inverting Amplifier:



- By rule #2, point A is V_{in} .
- By Rule #1, no current is going into the op amp.
- We can redraw the circuit as:

- The closed loop gain is $(R_1 + R_f) / R_1$.
- The output has the same polarity as the input.

• Integrating Amplifier:



• Again, using the two rules for op amp circuits we redraw the circuit as:

$$V_{\rm m} \xrightarrow{I_{\rm in} \rightarrow} \xleftarrow{I_{\rm out}}_{R_1} \xrightarrow{I_{\rm out}}_{R_1} V_{\rm out}$$
$$\frac{V_{\rm in}}{R_1} + \frac{dQ}{dt} = 0$$
$$\frac{V_{\rm in}}{R_1} + C \frac{dV_{\rm out}}{dt} = 0$$
$$V_{\rm out} = \frac{-1}{CR_1} \int V_{\rm in} dt$$

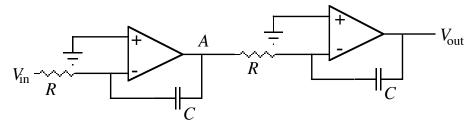
- The output voltage is related to the integral of the input voltage.
- The negative sign in the gain means that V_{in} and V_{out} have opposite polarity.

• Op Amps and Analog Calculations:

- Op amps were invented before transistors to perform analog calculations.
- Their main function was to solve differential equations in real time.
- Example: Suppose we wanted to solve the following:

$$\frac{d^2x}{dt^2} = g$$

- This describes a body under constant acceleration (gravity if $g = 9.8 \text{ m/s}^2$).
- The following circuit gives an output which is the solution to the differential equation:



0

- The input voltage is a constant (=g).
- For convenience we pick RC = 1.
- At point A:

$$V_{\rm A} = -\int V_{\rm in} dt = -\int \frac{d^2 x}{dt^2} dt = -\frac{dx}{dt}$$

The output voltage (V_{out}) is the integral of V_A : $V_{out} = -\int V_A dt = \int \frac{dx}{dt} dt = x(t)$

If we want non-zero boundary conditions (e.g. V(t = 0) = 1 m/s) we add a DC voltage at point A.