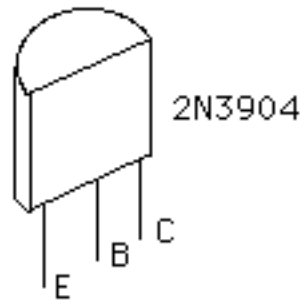
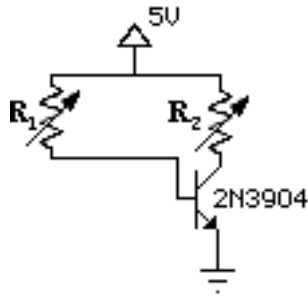


Physics 4700 Experiment 4  
Transistor Amplifier

1) Build the following circuit, with  $R_1 = 5\text{ M}\Omega$  and  $R_2 = 10\text{ k}\Omega$ . Vary  $I_B$  between 1 and  $30\text{ }\mu\text{A}$  and measure  $V_{CE}$  and  $I_C$ . Plot  $I_{C1}$ ,  $\beta (= h_{fe} = I_C / I_B)$ ,  $V_{CE}$ , vs.  $I_B$ . Compare your results with Fig. 11 (this figure has  $V_{CE}$  fixed at 10 V) of the 2N3904 spec sheet. What is the saturation current and saturation voltage ( $V_{CE}$  at saturation)?



2) Design a single stage common emitter amplifier. The amplifier should have the following specs:

- a) flat frequency response from 30 to 10 kHz (i.e. -3 dB point at 30 Hz)
- b) voltage gain of  $\approx 100$
- c) input impedance  $> 300\text{ }\Omega$

3) Measure the following properties of your amplifier and compare your results with expectations:

- a) DC voltages at operating point.
- b) plot voltage gain as a function of frequency (30-100 kHz).
- c) capture a picture of the amp's output response to a large input sine wave.

Suggested References:

Class notes of course.

Simpson Experiment 13 (P. 862) and 14 (P. 864).

Student Manual for Art of Electronics (most of Chapter 2).

### Designing the Common Emitter Amp

In this note I will outline a plan for designing a common emitter (CE) amplifier. There are many other ways of designing such an amp however they involve techniques beyond this class. Here are some good references on the subject:

Simpson: Section 5.7 (P. 221) and Experiment 14 (P. 865)

Diefenderfer: P. 152-154

Hayes and Horowitz: P. 115

A general purpose design for the CE amp is given in Fig. 1.

$R_1$  and  $R_2$  are bias resistors and are used to keep the transistor "turned on" for DC voltages ( $V_{cc}$ ).  $R_C$  and  $R_E$  determine the gain of the amp and  $R_E$  plays a role in determining the input impedance of the amp.  $C_E$  provides a path to ground for AC signals, while  $C_{in}$  and  $C_{out}$  isolate the input and output of the amp from the DC voltages that are present on the transistor.

*Some general rules to keep in mind:*

- a) Our transistor amp amplifies small signals, typically mV.
- b) Typical DC collector current is a few mA.
- c) The gain ( $V_{out}/V_{in}$ ) of a CE amp is  $\approx R_C/r_{BE}$  if  $R_E = 0$ .  $r_{BE}$  is intrinsic to the transistor. You can't touch it! It is given by:

$$r_{BE} = h_{ie}/h_{fe} \approx 25 \text{ mV}/I_C. \text{ So if } I_C = 1 \text{ mA then } r_{BE} = 25 \Omega.$$

(See Simpson P. 227, 244 or class notes or Hayes and Horowitz P. 113)

- d) The AC input impedance of the transistor is  $\approx \beta r_{BE}$  (or  $h_{fe} r_{be}$ ).

A typical  $\beta$  is 100. Remember that  $\beta = h_{fe} = I_C/I_B$  so for 1 mA of collector current the AC input impedance is  $\approx (100)(25) = 2500 \Omega$ .

- e) The DC input impedance of the transistor is  $\approx \beta R_E$  (or  $h_{fe} R_E$ ). A typical value of  $R_E$  is 1 k $\Omega$ . So the DC impedance is much larger (e.g. 100 k vs. 2.5 k) than the AC impedance.

- f) Since  $I_E = I_C + I_B$  and  $I_B = I_C/\beta$  we assume that  $I_C = I_E$  for design purposes.

- g) In order to stabilize the transistor from problems due to heating we should have:

$$R_1 \parallel R_2 < 10 R_E.$$

See Simpson (P. 215-221) or Diefenderfer (P. 148) for a discussion of thermal stability.

*With rules a-g in mind we are ready to design the CE amplifier.*

- 1) Pick  $V_{cc}$ . Let's use  $V_{cc} = 15$  Volts since all our lab supplies go up to this value.

- 2) We want the voltage gain  $G = V_{out}/V_{in} > 100$ . From rule c

$$G \approx R_C/r_E = R_C/(25 \Omega/I_C).$$

From the 2N3904 spec sheet (Fig. 2)  $I_C = 2.5$  mA looks like good place to operate the transistor (any choice in the linear region of the transistor would be OK):

$$G \approx R_C/10 > 100$$

$$R_C > 1000 \Omega$$

Pick  $R_C = 2000 \Omega$ .

3) We now need to decide what the maximum collect current ( $I_C$ ) we will allow. From the spec sheet 4 mA looks reasonable. Applying Kirchhoff's law to the circuit in Fig. 1 yields the following load line ( $I_C$  vs.  $V_{CE}$ ) equation:

$$I_C = V_{cc}/(R_E + R_C) - V_{CE}/(R_E + R_C)$$

(when  $I_C = 4$  mA,  $V_{CE} = 0$  Volts and when  $I_C = 0$  mA,  $V_{CE} = 15$  Volts)

$V_{CE} \approx 5-6$  Volts is in the linear region. From the spec sheet we see that  $I_B$  must be  $\approx 10$   $\mu$ A.

4) Using #3 from above we can find  $R_E$ .

$$I_C(\text{max}) = V_{cc}/(R_E + R_C) = 4 \text{ mA} = 15 \text{ V}/(2000 \text{ } \Omega + R_E)$$

$$R_E = 1.75 \text{ k}\Omega$$

5) We can now find  $V_E$  and thus  $V_B$ .

$$V_E = I_E R_E \approx I_C R_E = (2.5 \text{ mA})(1.75 \text{ k}\Omega)$$

$$V_E \approx 4.4 \text{ Volts}$$

Remember  $V_B = V_E + 0.6$  Volts for an NPN transistor.

$$V_B \approx 5 \text{ Volts}$$

6) We can now find  $R_1$  and  $R_2$  since:

$$V_B = [15 \text{ V}][R_2/(R_1 + R_2)] \text{ with } V_B = 5 \text{ V.}$$

From rule g on P. 1 we need  $R_1 \parallel R_2 < 10 R_E = 17.5 \text{ k}\Omega$ .

Also  $R_1$  and  $R_2$  must provide enough base current ( $I_B \approx 10$   $\mu$ A)

$$V_{cc}/(R_1 + R_2) \gg I_B \approx 10 \text{ } \mu\text{A.}$$

A choice of  $R_1$  and  $R_2$  that satisfies all of the above is:

$$R_1 = 10 \text{ k}\Omega \text{ and } R_2 = 5 \text{ k}\Omega. \text{ There are many other choices.}$$

7) The AC input impedance of the amp can now be calculated:

$$1/Z_{\text{input}} \approx 1/R_1 + 1/R_2 + 1/R_{\text{transistor}} = 1/(10 \text{ k}\Omega) + 1/(5 \text{ k}\Omega) + 1/R_{\text{transistor}}$$

$$R_{\text{transistor}} = \beta r_{BE} \approx 1 \text{ k}\Omega \text{ for } I_C = 2.5 \text{ mA, } \beta = 100 \text{ (see rule d).}$$

$$Z_{\text{input}} = 800 \text{ } \Omega.$$

8) We now need to find values for the three capacitors,  $C_E$ ,  $C_{\text{in}}$ , and  $C_{\text{out}}$ .

$C_E$  must provide an AC ground for the emitter so we must have:

$$X_{CE} = 1/(2\pi f C_E) \ll R_E = 1.75 \text{ k}\Omega.$$

Let  $X_{CE} = R_E/10$ . The lowest frequency we are concerned with is 30 Hz so:

$$C_E = 1/(2\pi f X_{CE}) = 1/(2\pi \times 30 \times (R_E/10)) = 30 \text{ } \mu\text{F.}$$

9) Finally we need to choose  $C_{\text{in}}$  and  $C_{\text{out}}$ . Pick these capacitors so we have the  $-3$  dB points at 30 Hz. Remember  $\omega_{3\text{dB}} = 1/RC$ . For the input  $R \approx 800 \text{ } \Omega$  and for the output  $R \approx 1 \text{ M}\Omega$  (scope resistance). Thus we have:

$$C_{\text{in}} \approx 1/(800 \text{ } \Omega \times 2\pi \times 30) = 6 \text{ } \mu\text{F}$$

$$C_{\text{out}} \approx 1/(1 \text{ M}\Omega \times 2\pi \times 30) = 0.005 \text{ } \mu\text{F}$$

We have now determined all  $R$ 's and  $C$ 's. When you build the circuit don't be too disappointed (or surprised) if your measurements are different than the above calculations. We used a very simple model of the transistor.

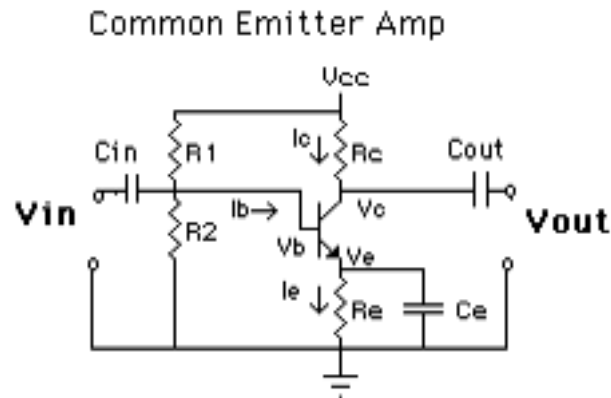


Fig. 1

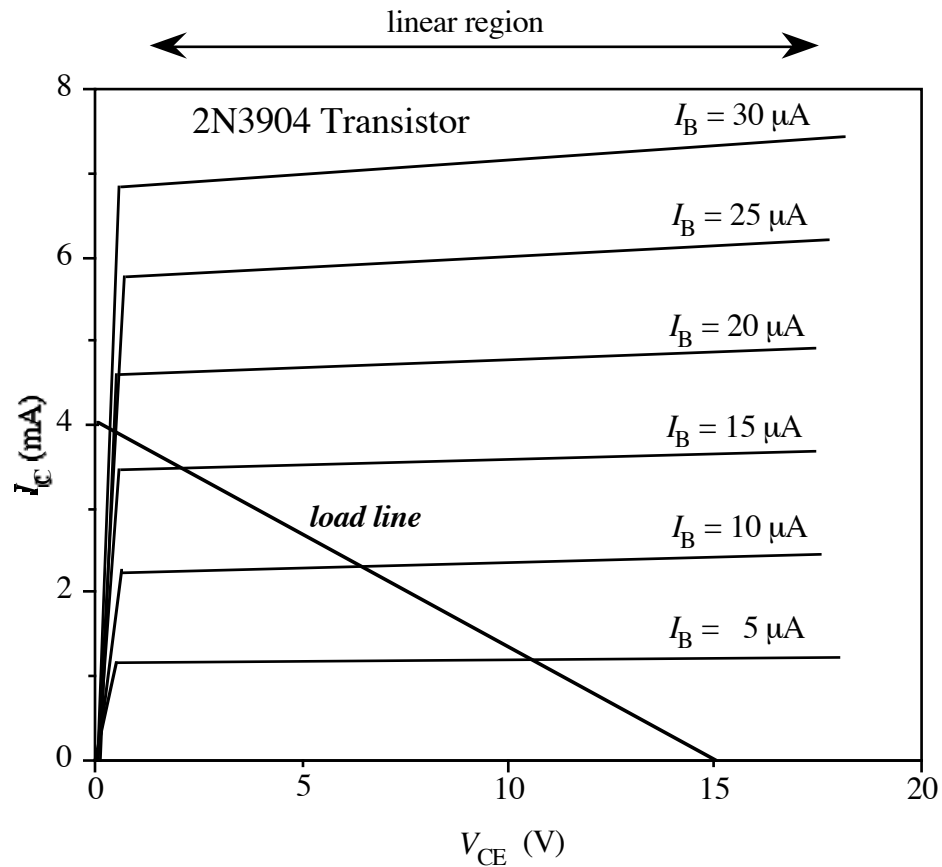


Fig. 2: 2N3904 Spec Sheet.