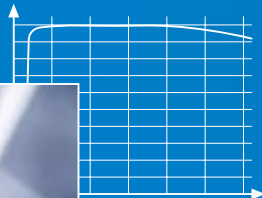


Optical Glass

Properties



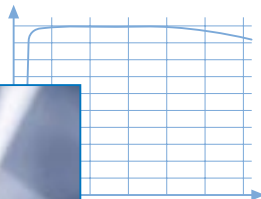
SCHOTT
glass made of ideas

Eigenschaften

Glascode	- Internationaler Glascode aus Brechzahl n_d und Abbezahl v_d mit Dichte
$n_x, v_x, n_x - n_y$	- Brechzahl, Abbezahl und Dispersion bei verschiedenen Wellenlängen
CR	- Klima-Resistenzklasse (ISO/WD 13384)
FR	- Flecken-Resistenzklasse
SR	- Säure-Resistenzklasse (ISO 8424)
AR	- Alkali-Resistenzklasse (ISO 10629)
PR	- Phosphat-Resistenzklasse (ISO 9689)
α	- Koeffizient der thermischen Längenausdehnung α (-30°C; +70°C) in $10^{-6}/K$
T_g	- Transformationstemperatur in °C (ISO 7884-8)
$T_{10}^{7,6}$	- Temperatur des Glases in °C bei einer Viskosität von $10^{7,6}$ dPa s
ρ	- Dichte in g/cm^3
HK	- Knoophärte (ISO 9385)
HG	- Schleifbarkeitsklasse (ISO 12844)
B	- Blasenklasse
τ_i	- Reintransmissionsgrad bei 400 nm; Glasdicke: 25 mm
Farbcode	- Wellenlängen für Transmission 0,80 bzw. 0,05; Glasdicke: 10 mm (JOGIS)

Optical Glass

Properties



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Glass type	n_d	v_d	$n_F - n_C$	n_e	v_e	$n_{F'} - n_{C'}$	n_r	n_C	$n_{F'}$	n_g	n_h
N-FK5 487704.245	1.48749	70.41	0.006924	1.48914	70.23	0.006965	1.48410	1.48535	1.49266	1.49593	1.49894
N-FK51 487845.373	1.48656	84.47	0.005760	1.48794	84.07	0.005804	1.48379	1.48480	1.49088	1.49364	1.49618
N-FK56 434950.354	1.43425	94.95	0.004573	1.43534	94.53	0.004606	1.43204	1.43285	1.43768	1.43986	1.44185
N-PK51 529770.396	1.52855	76.98	0.006867	1.53019	76.58	0.006923	1.52527	1.52646	1.53372	1.53704	1.54010
N-PK52 497816.376	1.49700	81.63	0.006088	1.49846	81.22	0.006137	1.49409	1.49515	1.50158	1.50451	1.50721
N-PSK3 552635.291	1.55232	63.46	0.008704	1.55440	63.23	0.008767	1.54811	1.54965	1.55885	1.56302	1.56688
N-PSK53 620635.360	1.62014	63.48	0.009769	1.62247	63.19	0.009851	1.61547	1.61717	1.62749	1.63223	1.63662
N-PSK57 592684.447	1.59240	68.40	0.008661	1.59447	68.01	0.008741	1.58830	1.58978	1.59894	1.60317	1.60708
N-PSK58 569712.440	1.56907	71.21	0.007992	1.57098	70.81	0.008063	1.56528	1.56665	1.57509	1.57899	1.58258

CR	FR	SR	AR	PR	α	Tg	T ₁₀ ^{7.6}	ρ	HK	HG	B	τ_i	FC
2	1	4	2	2.3	9.2	466	672	2.45	520	3	1	0.993	30/25
2	0	52.3	2.2	4.3	13.3	420		3.73	430	5	1	0.993	34/28
1	0	52.3	4.3	4.3		422		3.54	350		1	0.996	33/28
2	0	51.2	3.3	4.3	12.7	496		3.96	400	6	1	0.984	35/29
1	0	52.3	3.3	4.3	13.8	440	533	3.77	370	6	1	0.986	34/29
3	0	2.2	2	2	6.2	599	736	2.91	630	2	1	0.986	33/28
2	1	52.3	1.2	4.3	9.4	618	709	3.60	440	6	1	0.950	37/33
1	0	51.3	1.2	4.3	13.2	497		4.48	370		1	0.992	34/29
1	0	51.3	1.3	4.3	13.4	476		4.40	360		1	0.982	34/29

Glass type	n_d	v_d	$n_F - n_C$	n_e	v_e	$n_{F'} - n_{C'}$	n_r	n_C	$n_{F'}$	n_g	n_h
N-BK7 517642.251	1.51680	64.17	0.008054	1.51872	63.96	0.008110	1.51289	1.51432	1.52283	1.52668	1.53024
N-BK10 498670.239	1.49782	66.95	0.007435	1.49960	66.78	0.007481	1.49419	1.49552	1.50337	1.50690	1.51014
N-K5 522595.259	1.52249	59.48	0.008784	1.52458	59.22	0.008858	1.51829	1.51982	1.52910	1.53338	1.53734
K7 511604.253	1.51112	60.41	0.008461	1.51314	60.15	0.008531	1.50707	1.50854	1.51748	1.52159	1.52540
K10 501564.252	1.50137	56.41	0.008888	1.50349	56.15	0.008967	1.49713	1.49867	1.50807	1.51243	1.51649
N-ZK7 508612.249	1.50847	61.19	0.008310	1.51045	60.98	0.008370	1.50445	1.50592	1.51470	1.51869	1.52238

CR	FR	SR	AR	PR	α	Tg	T ₁₀ ^{7.6}	ρ	HK	HG	B	τ_i	FC
2	0	1	2	2.3	7.1	557	719	2.51	610	3	0	0.992	33/29
1	0	1	1	1	5.8	551	753	2.39	560	4	1	0.990	31/27
1	0	1	1	1	8.2	546	720	2.59	530	3	1	0.988	34/30
3	0	2	1	2.3	8.4	513	712	2.53	520		1	0.990	33/30
1	0	1	1	1.2	6.5	459	691	2.52	470	4	1	0.986	33/30
1	0	2	1.2	2.2	4.5	539	721	2.49	530	4	1	0.975	34/29

BK
K
ZK

Glass type	n_d	v_d	$n_F - n_C$	n_e	v_e	$n_{F'} - n_{C'}$	n_r	n_C	$n_{F'}$	n_g	n_h
N-BAK1 573575.319	1.57250	57.55	0.009948	1.57487	57.27	0.010039	1.56778	1.56949	1.58000	1.58488	1.58941
N-BAK2 540597.286	1.53996	59.71	0.009043	1.54212	59.44	0.009120	1.53564	1.53721	1.54677	1.55117	1.55525
N-BAK4 569560.304	1.56883	55.98	0.010162	1.57125	55.70	0.010255	1.56400	1.56575	1.57649	1.58149	1.58614
N-SK2 607567.355	1.60738	56.65	0.010722	1.60994	56.37	0.010821	1.60230	1.60414	1.61547	1.62073	1.62562
N-SK4 613586.353	1.61272	58.63	0.010450	1.61521	58.37	0.010541	1.60774	1.60954	1.62059	1.62568	1.63042
N-SK5 589613.330	1.58913	61.27	0.009616	1.59142	61.02	0.009692	1.58451	1.58619	1.59635	1.60100	1.60530
N-SK10 623570.366	1.62278	56.98	0.010931	1.62538	56.70	0.011030	1.61759	1.61947	1.63102	1.63638	1.64137
N-SK11 564608.308	1.56384	60.80	0.009274	1.56605	60.55	0.009349	1.55939	1.56101	1.57081	1.57530	1.57946
N-SK14 603606.344	1.60311	60.60	0.009953	1.60548	60.34	0.010034	1.59834	1.60008	1.61059	1.61542	1.61988
N-SK15 623580.362	1.62296	58.02	0.010737	1.62552	57.75	0.010832	1.61785	1.61970	1.63105	1.63629	1.64116

CR	FR	SR	AR	PR	α	Tg	T ₁₀ ^{7.6}	ρ	HK	HG	B	τ_i	FC
2	1	3.3	1.2	2	7.6	592	746	3.19	530		1	0.990	33/29
2	0	1	1	2.3	8.0	554	727	2.86	530	2	1	0.993	32/28
1	0	1.2	1	1	7.0	581	725	3.05	550	2	0	0.980	36/33
2	0	2.2	1	2.3	6.0	659	823	3.55	550	2	0	0.984	35/30
3	1	51.2	2	2	6.5	658	769	3.54	580	3	1	0.975	36/32
3	1	4.4	2	1.3	5.5	660	791	3.30	590	3	1	0.981	34/29
3	3	52.2	2	2.2		641	761	3.67	550		1	0.962	36/32
2	0	2	1	2.3	6.5	610	760	3.08	570		1	0.975	34/29
4	2	51.3	2	2.3	6.0	649	773	3.44	600	3	1	0.975	35/29
3	3	52.2	2	3.2	6.7	641	752	3.62	620	3	1	0.960	36/31

BAK
SK

Glass type	n_d	v_d	$n_F - n_C$	n_e	v_e	$n_{F'} - n_{C'}$	n_r	n_C	$n_{F'}$	n_g	n_h
N-SK16 620603.358	1.62041	60.32	0.010285	1.62286	60.08	0.010368	1.61548	1.61727	1.62814	1.63312	1.63773
N-SK18 639554.364	1.63854	55.42	0.011521	1.64128	55.15	0.011628	1.63308	1.63505	1.64724	1.65290	1.65819
SK51 621603.352	1.62090	60.31	0.010295	1.62335	60.02	0.010386	1.61600	1.61777	1.62866	1.63369	1.63836

CR	FR	SR	AR	PR	α	Tg	T ₁₀ ^{7.6}	ρ	HK	HG	B	τ_i	FC
4	4	53.3	3.3	3.2	6.3	636	750	3.58	600	4	1	0.970	36/30
3	4	52.3	2.2	3.3	6.4	643	751	3.64	610		1	0.950	37/33
2	3	52.3	1.3	4.3	8.9	597	684	3.52	450	3	1	0.958	36/31

Glass type	n_d	v_d	$n_F - n_C$	n_e	v_e	$n_{F'} - n_{C'}$	n_r	n_C	$n_{F'}$	n_g	n_h
N-KF9 523515.249	1.52346	51.54	0.010156	1.52588	51.26	0.010258	1.51867	1.52040	1.53114	1.53620	1.54096
N-BALF4 580539.311	1.57956	53.87	0.010759	1.58212	53.59	0.010863	1.57447	1.57631	1.58769	1.59301	1.59799
N-BALF5 547536.261	1.54739	53.63	0.010207	1.54982	53.36	0.010303	1.54255	1.54430	1.55510	1.56016	1.56491
N-SSK2 622533.352	1.62229	53.27	0.011681	1.62508	52.99	0.011795	1.61678	1.61877	1.63112	1.63691	1.64232
N-SSK5 658509.371	1.65844	50.88	0.012940	1.66152	50.59	0.013075	1.65237	1.65455	1.66824	1.67471	1.68079
N-SSK8 618498.326	1.61773	49.83	0.012397	1.62068	49.54	0.012529	1.61192	1.61401	1.62713	1.63335	1.63923
N-LAK7 652585.384	1.65160	58.52	0.011135	1.65425	58.26	0.011229	1.64628	1.64821	1.65998	1.66539	1.67042
N-LAK8 713538.374	1.71300	53.83	0.013245	1.71616	53.61	0.013359	1.70668	1.70897	1.72297	1.72944	1.73545

CR	FR	SR	AR	PR	α	Tg	T ₁₀ ^{7.6}	ρ	HK	HG	B	τ_i	FC
1	0	1	1	1	9.6	476	640	2.50	480	1	1	0.965	37/34
1	0	1	1	1	6.5	578	661	3.11	540	2	1	0.964	37/33
1	0	1	2	1	7.3	558	711	2.61	600	2	1	0.957	37/34
1	0	1.2	1	1	5.8	653	801	3.53	570	3	1	0.954	37/33
2	3	52.2	2.2	3.2	6.8	645	751	3.71	590	5	1	0.900	38/34
1	0	1	1.3	1	7.2	616	742	3.27	570	3	1	0.880	39/35
3	2	53.3	3.3	4.3	7.1	618	716	3.84	600		0	0.943	37/30
3	2	52.3	1	3.3	5.6	643	717	3.75	740	2	0	0.943	37/30

KF
BALF
SSK
LAK

Glass type	n_d	v_d	$n_F - n_C$	n_e	v_e	$n_{F'} - n_{C'}$	n_r	n_C	$n_{F'}$	n_g	n_h
N-LAK9 691547.351	1.69100	54.71	0.012631	1.69401	54.48	0.012738	1.68497	1.68716	1.70051	1.70667	1.71239
N-LAK10 720506.368	1.72003	50.62	0.014224	1.72341	50.39	0.014357	1.71328	1.71572	1.73077	1.73779	1.74438
N-LAK12 678552.410	1.67790	55.20	0.012281	1.68083	54.92	0.012396	1.67209	1.67419	1.68717	1.69320	1.69882
LAKL12 678549.332	1.67790	54.92	0.012342	1.68084	54.69	0.012450	1.67201	1.67415	1.68720	1.69322	1.69882
LAKN13 694533.424	1.69350	53.33	0.013004	1.69660	53.05	0.013131	1.68737	1.68958	1.70333	1.70975	1.71573
N-LAK14 697554.363	1.69680	55.41	0.012575	1.69980	55.19	0.012679	1.69077	1.69297	1.70626	1.71237	1.71804
N-LAK21 640601.374	1.64049	60.10	0.010657	1.64304	59.86	0.010743	1.63538	1.63724	1.64850	1.65366	1.65844
N-LAK22 651559.373	1.65113	55.89	0.011650	1.65391	55.63	0.011755	1.64560	1.64760	1.65992	1.66562	1.67092
N-LAK33 754524.426	1.75398	52.43	0.014381	1.75740	52.20	0.014510	1.74714	1.74962	1.76482	1.77187	1.77843
N-LAK34 729547.											

CR	FR	SR	AR	PR	α	Tg	T ₁₀ ^{7.6}	ρ	HK	HG	B	τ_i	FC
3	3	52	1.2	4.3	6.3	656	722	3.51	700		0	0.950	37/30
2	2	52.3	1	3	5.7	636	714	3.69	780	2	0	0.900	39/34
3	1	53.3	3.3	4.3	7.6	614	714	4.10	560	6	1	0.940	37/31
3	3	53.3	2.2	3.3	6.8	636	764	3.32	700	2	0	0.953	37/30
2	2	53.1	2.3	4	8.4	614	718	4.24	560	6	1	0.954	37/31
3	2	52.3	1	3	5.5	661	734	3.63	730		0	0.940	37/29
4	2	53.2	4.3	4.3	6.8	639	716	3.74	600	5	0	0.950	37/31
2	2	51.2	1	2.3	6.6	689		3.73	600	4	0	0.964	36/30
1	1	51.3	1	2.3	6.0	652		4.26	780	2	1	0.910	39/32

Glass type	n_d	v_d	$n_F - n_C$	n_e	v_e	$n_{F'} - n_{C'}$	n_r	n_C	$n_{F'}$	n_g	n_h
LLF1 548458.294	1.54814	45.75	0.011981	1.55099	45.47	0.012118	1.54256	1.54457	1.55725	1.56333	1.56911
N-LLF1 548459.249	1.54814	45.85	0.011955	1.55098	45.55	0.012095	1.54258	1.54458	1.55724	1.56336	1.56924
N-LLF6 532489.249	1.53169	48.90	0.010874	1.53427	48.61	0.010990	1.52659	1.52843	1.53993	1.54541	1.55061
N-BAF3 583466.279	1.58272	46.64	0.012495	1.58569	46.35	0.012637	1.57689	1.57899	1.59222	1.59857	1.60463
N-BAF4 606437.288	1.60568	43.72	0.013853	1.60897	43.43	0.014021	1.59926	1.60157	1.61624	1.62336	1.63022
N-BAF10 670471.374	1.67003	47.11	0.014222	1.67341	46.83	0.014380	1.66339	1.66578	1.68083	1.68801	1.69480
N-BAF51 652450.333	1.65224	44.96	0.014507	1.65569	44.67	0.014677	1.64551	1.64792	1.66328	1.67065	1.67766
N-BAF52 609466.304	1.60863	46.60	0.013061	1.61173	46.30	0.013211	1.60254	1.60473	1.61856	1.62521	1.63157

CR	FR	SR	AR	PR	α	Tg	T ₁₀ ^{7.6}	ρ	HK	HG	B	τ_i	FC
1	0	1	2	1	8.1	448	628	2.94	450	3	1	0.993	33/31
1	0	1	1	1	8.0	532	729	2.49	520	3	1	0.925	38/35
1	0	1	1	1	7.7	489	668	2.50	520	2	1	0.955	37/34
1	0	1	1	1	7.2	583	714	2.79	560	2	1	0.900	39/35
1	0	1	1.2	1.3	7.2	580	709	2.89	610	3	1	0.870	39/35
1	0	4.3	1.3	1	6.2	660	790	3.75	620	4	1	0.880	39/35
2	0	5.4	1.3	1	8.4	569	712	3.33	560	5	1	0.890	39/34
1	0	1	1.3	1	6.9	594	723	3.05	600	3	1	0.880	39/35

LLF
BAF

Glass type	n_d	v_d	$n_F - n_C$	n_e	v_e	$n_{F'} - n_{C'}$	n_r	n_C	$n_{F'}$	n_g	n_h
N-LF5 581408.257	1.58144	40.85	0.014234	1.58481	40.56	0.014417	1.57489	1.57723	1.59231	1.59970	1.60685
LF5 581409.322	1.58144	40.85	0.014233	1.58482	40.57	0.014413	1.57489	1.57723	1.59231	1.59964	1.60668
N-F2 620364.265	1.62005	36.43	0.017020	1.62408	36.16	0.017258	1.61229	1.61506	1.63310	1.64209	1.65087
F2 620364.361	1.62004	36.37	0.017050	1.62408	36.11	0.017284	1.61227	1.61503	1.63310	1.64202	1.65064
F4 617366.358	1.61659	36.63	0.016834	1.62058	36.37	0.017064	1.60891	1.61165	1.62949	1.63828	1.64679
F5 603380.347	1.60342	38.03	0.015867	1.60718	37.77	0.016078	1.59616	1.59875	1.61556	1.62381	1.63176

CR	FR	SR	AR	PR	α	Tg	T ₁₀ ^{7.6}	ρ	HK	HG	B	τ_i	FC
1	0	1	1	1	8.0	579	729	2.57	550	1	1	0.860	39/36
2	0	1	2.3	2	9.1	419	585	3.22	450	2	1	0.992	34/31
1	0	1	1	1	7.8	566	688	2.65	600	2	1	0.870	39/36
1	0	1	2.3	1.3	8.2	432	593	3.61	420	2	0	0.984	35/32
1	0	1	2.3	2	8.3	436	614	3.58	420		1	0.971	35/33
1	0	1	2.3	2	8.0	438	608	3.47	450	3	1	0.984	35/32

Glass type	n_d	v_d	$n_F - n_C$	n_e	v_e	$n_{F'} - n_{C'}$	n_r	n_C	$n_{F'}$	n_g	n_h
N-BASF2 664360.315	1.66446	36.00	0.018457	1.66883	35.73	0.018720	1.65607	1.65905	1.67862	1.68838	1.69792
N-BASF51 724381.											
BASF51 724381.431	1.72373	38.11	0.018990	1.72823	37.85	0.019240	1.71503	1.71813	1.73825	1.74810	1.75759
N-BASF64 704394.320	1.70400	39.38	0.017875	1.70824	39.12	0.018105	1.69578	1.69872	1.71765	1.72690	1.73581

CR	FR	SR	AR	PR	α	Tg	T ₁₀ ^{7.6}	ρ	HK	HG	B	τ_i	FC
1	0	1	1	1	7.1	619	766	3.15	580	3	1	0.750	41/36
2	4	52.3	1.2	3.3	5.4	522	630	4.31	540	1	1	0.880	39/34
1	0	3.2	1.2	1	7.3	582	712	3.20	650	4	0	0.820	40/35

Glass type	n_d	v_d	$n_F - n_C$	n_e	v_e	$n_{F'} - n_{C'}$	n_r	n_C	$n_{F'}$	n_g	n_h
N-LAF2 744449.429	1.74397	44.85	0.016588	1.74791	44.57	0.016780	1.73627	1.73903	1.75659	1.76500	1.77298
N-LAF3 717480.414	1.71700	47.96	0.014950	1.72055	47.68	0.015112	1.71001	1.71252	1.72834	1.73585	1.74293
N-LAF7 749348.373	1.74950	34.82	0.021525	1.75459	34.56	0.021833	1.73972	1.74320	1.76602	1.77741	1.78854
LAFN7 750350.438	1.74950	34.95	0.021445	1.75458	34.72	0.021735	1.73970	1.74319	1.76592	1.77713	1.78798
N-LAF21 788475.434	1.78800	47.49	0.016594	1.79195	47.24	0.016763	1.78019	1.78301	1.80056	1.80883	1.81659
N-LAF32 795455.432	1.79457	45.53	0.017453	1.79872	45.28	0.017640	1.78640	1.78934	1.80780	1.81656	1.82482
N-LAF33 786441.436	1.78582	44.05	0.017839	1.79007	43.80	0.018038	1.77751	1.78049	1.79937	1.80837	1.81687
N-LAF34 773496.424	1.77250	49.62	0.015568	1.77621	49.38	0.015719	1.76515	1.76780	1.78427	1.79196	1.79915
N-LAF35 743492.											
N-LAF36 800423.											

CR	FR	SR	AR	PR	α	Tg	T ₁₀ ^{7.6}	ρ	HK	HG	B	τ_i	FC
2	3	52.2	1	2.2	8.1	653	742	4.30	530	6	1	0.840	40/34
2	3	52.3	1.2	3.3	7.6	646	740	4.14	580	5	1	0.890	39/34
1	2	51.3	1.2	1.2	7.3	568	669	3.73	530	5	1	0.490	46/36
3	1	53.3	2.2	4.3	5.3	500	573	4.38	520	3	0	0.850	40/35
1	1	51.3	1	1.3	6.2	663	724	4.34	780	2	1	0.880	40/33
1	1	51.2	1	2	5.9	643		4.33	760	2	1	0.860	40/34
1	2	52.2	1	3	5.6	600	673	4.36	730	1	0	0.895	39/32
1	1	51.3	1	1	5.8	668	745	4.24	770	2	0	0.930	38/32

LAF

Glass type	n_d	v_d	$n_F - n_C$	n_e	v_e	$n_{F'} - n_{C'}$	n_r	n_C	$n_{F'}$	n_g	n_h
LASFN9 850322.444	1.85025	32.17	0.026430	1.85651	31.93	0.026827	1.83834	1.84256	1.87059	1.88467	1.89844
N-LASF31 881410.541	1.88067	41.01	0.021475	1.88577	40.76	0.021731	1.87074	1.87429	1.89702	1.90793	1.91824
N-LASF35 1022291.541	2.02204	29.06	0.035170	2.03035	28.84	0.035721	2.00628	2.01185	2.04916	2.06805	2.08663
N-LASF40 834373.454	1.83404	37.30	0.022363	1.83935	37.04	0.022658	1.82380	1.82745	1.85114	1.86275	1.87393
N-LASF41 835431.493	1.83501	43.13	0.019361	1.83961	42.88	0.019578	1.82599	1.82923	1.84972	1.85949	1.86872
N-LASF43 806406.433	1.80610	40.61	0.019850	1.81081	40.36	0.020089	1.79691	1.80020	1.82122	1.83137	1.84106
N-LASF44 804465.447	1.80420	46.50	0.017294	1.80832	46.25	0.017476	1.79609	1.79901	1.81731	1.82594	1.83405
N-LASF45 801351.360	1.80100	35.08	0.022834	1.80641	34.83	0.023155	1.79062	1.79431	1.81851	1.83052	1.84218
N-LASF46 901315.											

CR	FR	SR	AR	PR	α	Tg	T ₁₀ ^{7.6}	ρ	HK	HG	B	τ_i	FC
2	0	2	1	1	7.4	698	825	4.44	630	4	1	0.563	49/35
1	0	2	1	1	6.8	758		5.41	770	2	1	0.820	45/32
1	0	1.3	1.0	1.3	7.4	774		5.41	810		1	0.12	-/38
1	1	51.2	1	2	5.8	585	673	4.55	690	1	0	0.750	44/35
1	0	4	1	1	6.2	668	742	4.93	760	1	0	0.876	41/32
1	1	51.3	1	2	5.6	614		4.33	720	1	0	0.810	42/34
1	1	4.3	1	1.3	6.2	662	742	4.47	770	1	0	0.910	40/31
1	0	3.3	1	1	7.3	651	767	3.60	670		0	0.710	44/35

LASF

Glass type	n_d	v_d	$n_F - n_C$	n_e	v_e	$n_{F'} - n_{C'}$	n_r	n_C	$n_{F'}$	n_g	n_h
N-SF1 717296.302	1.71736	29.62	0.024219	1.72308	29.39	0.024606	1.70651	1.71035	1.73605	1.74919	1.76224
SF1 717295.446	1.71736	29.51	0.024307	1.72310	29.29	0.024687	1.70647	1.71031	1.73610	1.74916	1.76201
SF2 648338.386	1.64769	33.85	0.019135	1.65222	33.60	0.019412	1.63902	1.64210	1.66238	1.67249	1.68233
N-SF4 755274.314	1.75513	27.38	0.027583	1.76164	27.16	0.028044	1.74286	1.74719	1.77647	1.79158	1.80668
SF4 755276.479	1.75520	27.58	0.027383	1.76167	27.37	0.027829	1.74300	1.74730	1.77636	1.79121	1.80589
N-SF5 673323.285	1.67271	32.25	0.020858	1.67763	32.00	0.021177	1.66330	1.66664	1.68876	1.69998	1.71106
SF5 673322.407	1.67270	32.21	0.020885	1.67764	31.97	0.021195	1.66327	1.66661	1.68876	1.69986	1.71069
N-SF6 805254.337	1.80518	25.36	0.031750	1.81266	25.16	0.032304	1.79114	1.79608	1.82980	1.84738	1.86506
SF6 805254.518	1.80518	25.43	0.031660	1.81265	25.24	0.032201	1.79117	1.79609	1.82970	1.84707	1.86436
N-SF8 689313.290	1.68894	31.31	0.022005	1.69413	31.06	0.022346	1.67904	1.68254	1.70589	1.71775	1.72948
N-SF10 728285.305	1.72828	28.53	0.025524	1.73430	28.31	0.025941	1.71688	1.72091	1.74800	1.76191	1.77578

CR	FR	SR	AR	PR	α	Tg	T ₁₀ ^{7.6}	ρ	HK	HG	B	τ_i	FC
1	0	1	1	1	9.1	553	660	3.03	540	5	1	0.700	41/36
2	1	3.2	2.3	3	8.1	417	566	4.46	390	1	1	0.920	39/34
1	0	2	2.3	2	8.4	441	600	3.86	410	2	0	0.954	37/33
1	0	1.3	1	1	9.5	570	661	3.15	520	6	1	0.550	44/37
1	2	4.3	2.3	3.3	8.0	420	552	4.79	390	1	1	0.890	40/35
1	0	1	1	1	7.9	578	693	2.86	620	3	1	0.780	40/36
1	1	2	2.3	3	8.2	425	580	4.07	410	2	1	0.950	37/33
1	0	2	1	1	9.0	594	694	3.37	550	4	1	0.570	45/37
2	3	51.3	2.3	3.3	8.1	423	538	5.18	370		0	0.760	42/36
1	0	1	1	1	8.6	567	678	2.90	600	4	1	0.770	41/36
1	0	1	1	1	9.4	559	652	3.05	540	5	1	0.640	42/36

SF

Glass type	n_d	v_d	$n_F - n_C$	n_e	v_e	$n_{F'} - n_{C'}$	n_r	n_C	$n_{F'}$	n_g	n_h
SF10 728284.428	1.72825	28.41	0.025633	1.73430	28.19	0.026051	1.71681	1.72085	1.74805	1.76198	1.77579
SF11 785258.474	1.78472	25.76	0.030467	1.79190	25.55	0.030997	1.77125	1.77599	1.80834	1.82518	1.84208
N-SF14 762265.											
SF14 762265.454	1.76182	26.53	0.028719	1.76859	26.31	0.029211	1.74910	1.75357	1.78407	1.79989	1.81573
N-SF15 699302.292	1.69892	30.20	0.023142	1.70438	29.96	0.023511	1.68854	1.69222	1.71677	1.72933	1.74182
SF15 699301.406	1.69895	30.07	0.023246	1.70444	29.83	0.023612	1.68853	1.69221	1.71688	1.72940	1.74176
N-SF56 785261.328	1.78470	26.10	0.030071	1.79179	25.89	0.030587	1.77137	1.77607	1.80800	1.82460	1.84126
SF56A 785261.492	1.78470	26.08	0.030092	1.79180	25.87	0.030603	1.77136	1.77605	1.80800	1.82449	1.84092
SFL57 847236.355	1.84666	23.62	0.035841	1.85510	23.43	0.036489	1.83089	1.83643	1.87451	1.89456	1.91488
N-SF57 847238.											
SF57 847238.551	1.84666	23.83	0.035536	1.85504	23.64	0.036166	1.83102	1.83650	1.87425	1.89393	1.91366

CR	FR	SR	AR	PR	α	Tg	T ₁₀ ^{7.6}	ρ	HK	HG	B	τ_i	FC
1	0	1	1.2	2	7.5	454	595	4.28	430	1	0	0.690	41/37
1	0	1	1.2	1	6.1	503	635	4.74	450	1	1	0.200	44/39
1	0	1	1.2	1	6.6	478	617	4.54	430	1	1	0.280	43/38
1	0	1	1	1	8.0	580	692	2.92	610	3	1	0.680	42/37
1	0	1	1.2	2.3	7.9	455	595	4.06	420	2	1	0.780	40/37
1	0	1	1.3	1	8.7	592	691	3.28	560	5	1	0.570	44/37
1	1	3.2	2.2	3.2	7.9	429	556	4.92	380	1	1	0.680	42/37
1	0	1.3	1	1.3	8.7	598	700	3.55	580		1	0.200	51/38
2	5	52.3	2.3	4.3	8.3	422	519	5.51	350	1	0	0.660	44/37

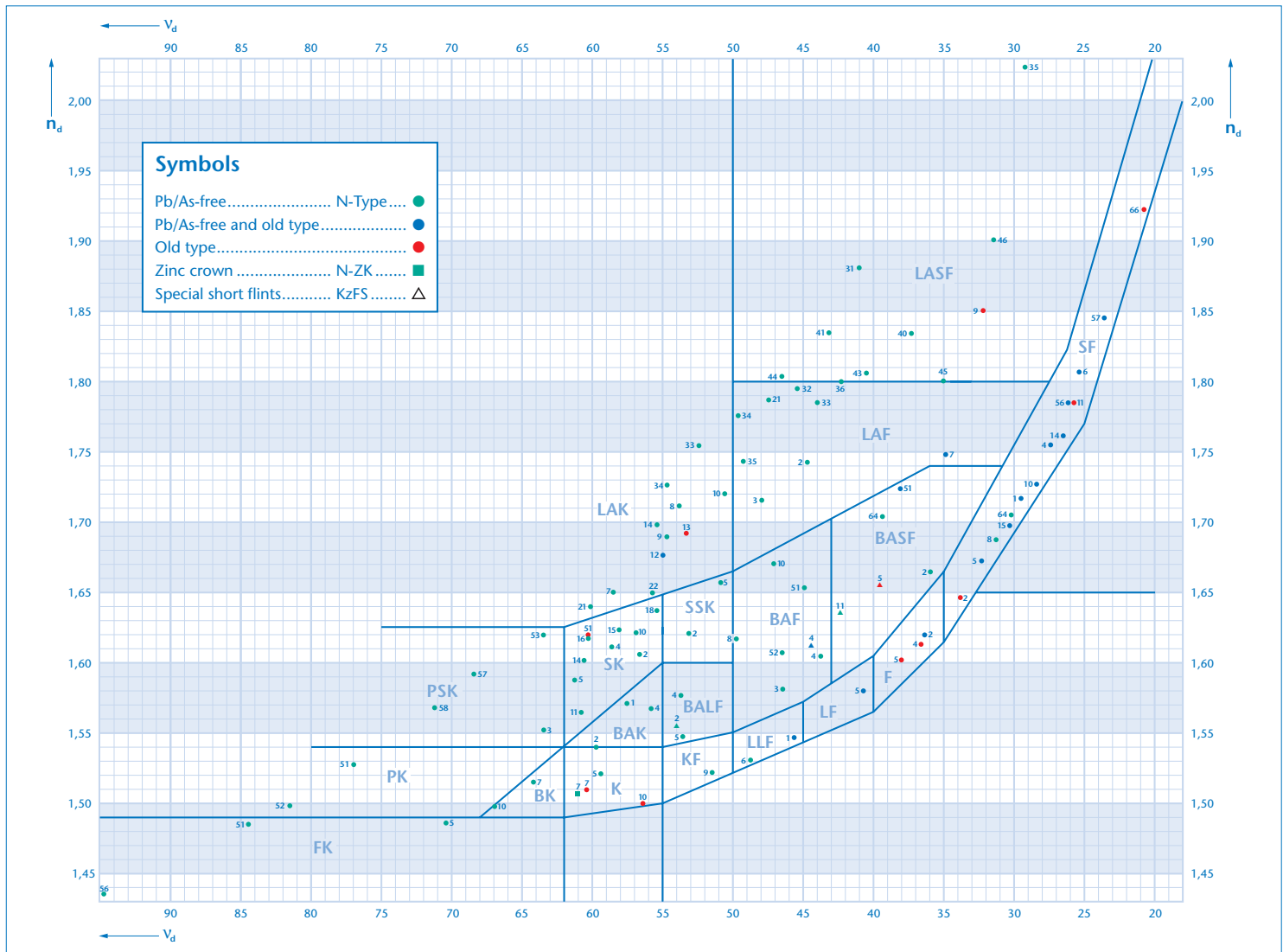
Glass type	n_d	v_d	$n_F - n_C$	n_e	v_e	$n_{F'} - n_{C'}$	n_r	n_C	$n_{F'}$	n_g	n_h
N-SF64 706302.298	1.70591	30.23	0.023350	1.71142	29.99	0.023720	1.69544	1.69914	1.72392	1.73657	1.74912
SF66 923209.602	1.92286	20.88	0.044189	1.93325	20.73	0.045030	1.90361	1.91033	1.95730	1.98229	2.00775

CR	FR	SR	AR	PR	α	Tg	T ₁₀ ^{7.6}	ρ	HK	HG	B	τ_i	FC
1	0	1	1.2	1	8.5	572	688	2.99	620	4	1	0.670	42/37
2	5	53.4	2.3	4.2	9.0	384	482	6.03	310	2	1	0.240	48/38

Glass type	n_d	v_d	$n_F - n_C$	n_e	v_e	$n_{F'} - n_{C'}$	n_r	n_C	$n_{F'}$	n_g	n_h
N-KZFS2 558540.255	1.55836	54.01	0.010338	1.56082	53.83	0.010418	1.55337	1.55519	1.56612	1.57114	1.57580
N-KZFS4 613445.300	1.61336	44.49	0.013785	1.61664	44.27	0.013929	1.60688	1.60922	1.62380	1.63071	1.63723
KZFSN4 613443.320	1.61340	44.29	0.013848	1.61669	44.07	0.013994	1.60689	1.60924	1.62389	1.63085	1.63745
KZFSN5 654396.346	1.65412	39.63	0.016507	1.65803	39.40	0.016701	1.64644	1.64920	1.66668	1.67512	1.68319
N-KZFS11 638424.319	1.63775	42.41	0.015038	1.64132	42.20	0.015198	1.63069	1.63324	1.64915	1.65670	1.66385

CR	FR	SR	AR	PR	α	Tg	T ₁₀ ^{7.6}	ρ	HK	HG	B	τ_i	FC
1	4	52.3	4.3	4.2	4.4	491	600	2.55	490	3	1	0.963	34/30
1	1	3.4	1.2	1	7.3	547	675	3.00	520	3	1	0.948	36/32
3	2	52.3	4.3	4.3	4.5	492	594	3.20	450		1	0.974	36/30
3	2	52.3	4.3	4.3	4.5	501		3.46	460	5	1	0.940	37/34
1	1	3.4	1	1	6.6	551		3.20	530		1	0.968	36/30

KZFS



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Abbe-Diagram

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